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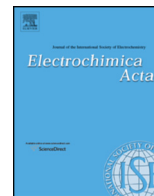


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Toward uniform electrodeposition of magnetic Co-W mesowires arrays: direct versus pulse current deposition



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ABSTRACT

Template-assisted electrodeposition of Co-rich Co-W alloys into mesoporous anodized aluminum oxide from ammonia-free solutions is investigated. The optimum deposition conditions rendering uniform filling of the pores, either by direct current (DC) or pulse current (PC) methods, are established. Contrary to the DC deposition on flat surfaces (which is kinetically controlled), the DC electrodeposition in the mesopores of the template is limited by mass transfer. Conversely, under PC mode, the Co-W electrodeposition process is controlled by kinetics at frequencies > 0.3 Hz; and by diffusion at lower frequencies. The obtained mesowires are nanocrystalline and exhibit a hexagonal closed packed (hcp) structure. The magnetic properties of selected Co-W mesowires, with variable aspect ratio, are also studied. The arrays of mesowires exhibit a semi-hard ferromagnetic behavior with coercivity values that surpass those of Co mesowires with similar dimensions. The interplay between interwire dipolar interactions, magnetocrystalline anisotropy and shape anisotropy on the overall shape of the hysteresis loops (in particular, on the coercivity and squareness ratio values, as well as on the effective magnetic easy axis direction) is investigated in a semiquantitative manner.

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1. Introduction

Magnetic metallic wires have received a remarkable interest in the last few years due to their potential applications in devices such as tunable microwave filters [1,2], miniaturized magnetic sensors based on the giant magnetoresistance (GMR) effect [3–5] or magnetic recording media with perpendicular-to-plane effective anisotropy [6,7], among others. The implementation of efficient large-scale synthesis methods that allow the mass production of different types of metallic wires in a homogeneous and reproducible manner is essential to cope with the current technological needs in all the aforementioned areas. Electrodeposition inside porous templates is a rather convenient and industrially scalable technique for the fabrication of micro-, meso-, nano-structures, not only wires, but also rods or tubes. Advantages of electrodeposition over other synthetic methods (e.g. electrospinning or lithographic procedures) include: ease of

operation and time-effectiveness, strict control of the wire length, precise tuning of the chemical composition and microstructure (i.e., crystallinity), and possibility to produce multilayered wires consisting of different segments with dissimilar compositions along the wire length [8].

For the growth of electrodeposited wires, either direct current or pulse plating conditions can be utilized. However, during direct current (or direct potential) electrodeposition, diffusion limitation effects can be quite prominent, hence causing a depletion of the metal ion concentration and/or a variation of pH at the bottom of the recesses. As a consequence, changes in the growing direction from nearly parallel to perpendicular to the wire axis, as well as changes in the crystal orientation of the wires can occur, thereby inducing variations in the resulting magnetic properties [9,10]. Pulse electrodeposition can be employed in order to minimize variations of pH and metal ion concentration in the course of electrodeposition, therefore overcoming the aforementioned problems. Furthermore, during electrodeposition at constant potential, simultaneously to the growth of the alloy in the recess, hydrogen evolves continuously and blocks the central part of the pores, thus shielding the deposition from the pore centre. Under these conditions, nanotubes are often formed. Conversely, in pulse

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potential mode, the evolved hydrogen has time to withdraw out of the pore during the pause time and the alloy can fill up the whole volume of the pore, resulting in the growth of fully dense wires.

The experimental conditions employed during pulse electro-deposition have a strong influence on the magnetic properties of the deposits [9]. Pulse plating has been satisfactorily used by several authors to fill all the pores of anodic aluminum oxide (AAO) templates with various metal nanowires (e.g., Ni or Co) [11,12]. During the study of Co [4–7,13–20], Ni [5,16,19,21–23], and their alloys [24–26] it was concluded that the quality of the resulting wires strongly depends on the duty cycle. A relatively long pause between the pulses is preferable. Also, the magnetic behavior of nanowire arrays differs from that of continuous microcrystalline deposits. The wire aspect ratio and the interwire distance have an influence on the magnetic properties since both parameters control the magnetic dipolar interactions in the array [4,6,7,15–18,27]. Finally, in order to use nanowires/nanotubes in widespread devices, the materials should not only possess tunable magnetic properties but also acceptable wear and corrosion resistance. Also, the length of the electrodeposited wires/tubes must be uniform.

In this work, Co-W mesowires have been grown inside porous AAO templates (pore diameter ~ 240 nm), given the remarkable mechanical, magnetic and tribological properties of this alloy when deposited onto flat surfaces [28–30]. The possibility to fabricate Co-W nanostructures inside the pores of AAO from citrate-ammonia solutions was demonstrated in [31]. At constant potential mode, only tubes were typically obtained, whereas wires were formed during deposition using pulse potential mode. As aforementioned, this difference in the shape of the nanostructures can be understood by the different hydrogen evolution inside the recesses in each case. Moreover, problems were noticed to maintain a constant pH in ammonia-containing solutions during long-lasting electrodeposition at elevated temperatures [32].

The aim of the present study is two-fold. On the one hand, the template-assisted electrodeposition of Co-W alloys into mesoporous AAO from ammonia-free solutions is investigated, and the best conditions rendering uniform filling of the pores are established. A citrate bath for Co-W electrodeposition was selected based on successful results observed during deposition of Co-W

alloys at 60 °C and pH 5.0, 6.7, and 8.0 on flat surfaces [28,33] and wafers [34]. On the other hand, the magnetic properties of best-quality Co-W mesowires, with variable aspect ratio, are also reported. The arrays of mesowires exhibit a semi-hard ferromagnetic behavior with coercivity values that surpass those of Co mesowires with similar dimensions.

2. Experimental

2.1. Template-assisted deposition of mesowires

Co-W mesowires were obtained by electrodeposition from a citrate electrolyte containing (mol L^{-1}): CoSO_4 –0.2; Na_2WO_4 –0.2; $\text{C}_6\text{H}_8\text{O}_7$ –0.04; $\text{Na}_3\text{C}_6\text{H}_5\text{O}_7$ –0.25; H_3BO_3 –0.65 under stagnant conditions. The pH was adjusted to 5.0, 6.7 and 8.0 by the addition of either H_2SO_4 or NaOH. Bath temperature was maintained at 20, 40, or 60 ± 2 °C.

The electrodeposition was performed using an Autolab PGSTAT302N system with an Ag/AgCl reference electrode. The counter electrode was a Pt mesh and the working electrode was a commercial Whatman AAO membrane with average pore-diameter of 240 nm and thickness of 60 μm . A Au layer was sputtered at the filter side to ensure the electrical contact (Au sputtered layer thickness was ~ 500 nm). The working area was estimated taking into account 50% porosity of AAO template.

Prior to electrodeposition, the working electrode was immersed in the electrolyte for several minutes under ultrasonic agitation in order to remove blocked gases and thereby improve electrolyte penetration into the pores. After the electrodeposition of Co-W mesowires, samples were rinsed with distilled water, ethanol and finally dried.

Co-W wire arrays were fabricated under: (i) potentiostatic mode at a constant cathodic potential $-E$ ranging from 0.8 to 1.1 V; (ii) galvanostatic mode at a constant cathodic current density $-i$ from 6 to 12 mA cm^{-2} ; (iii) pulse current (PC) mode at pulse duration (t_{on}) from 4 to 2000 ms, pulse cathodic current density ($-i_{\text{on}}$) from 7.5 to 60 mA cm^{-2} and duty cycles γ from 20 to 50%, where $\gamma = \frac{t_{\text{on}}}{t_{\text{on}} + t_{\text{off}}} \cdot 100\%$.

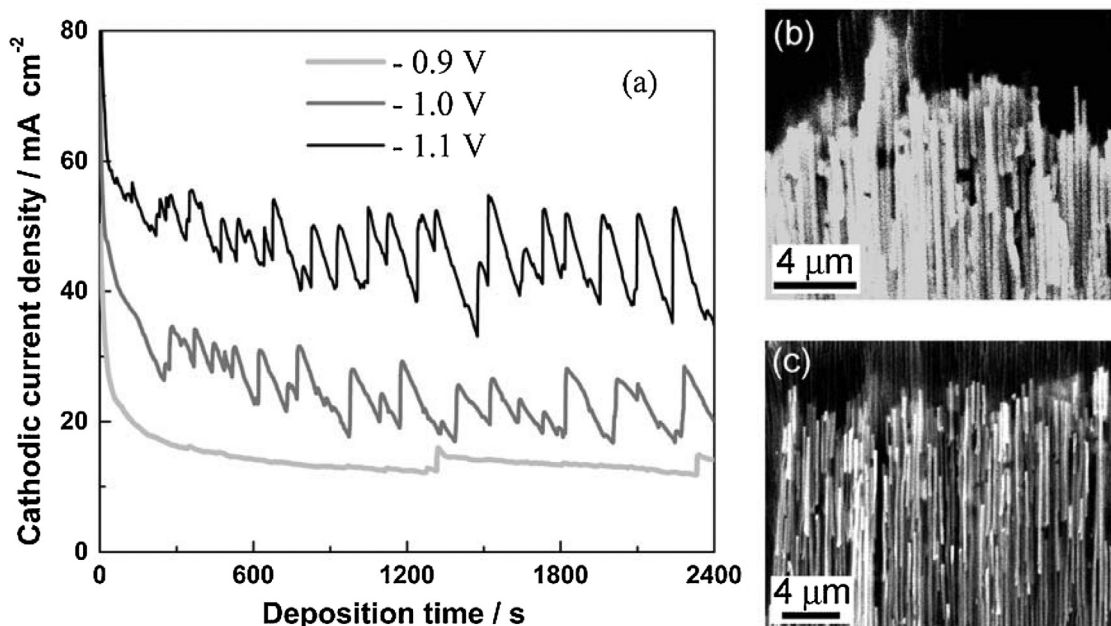


Fig. 1. (a) Chronoamperograms of Co-W mesowires deposition into AAO at pH=5 and 60 °C and SEM cross-section images corresponding to (b) -1.0 V and 2880s and (c) -0.9 V and 2667 s.

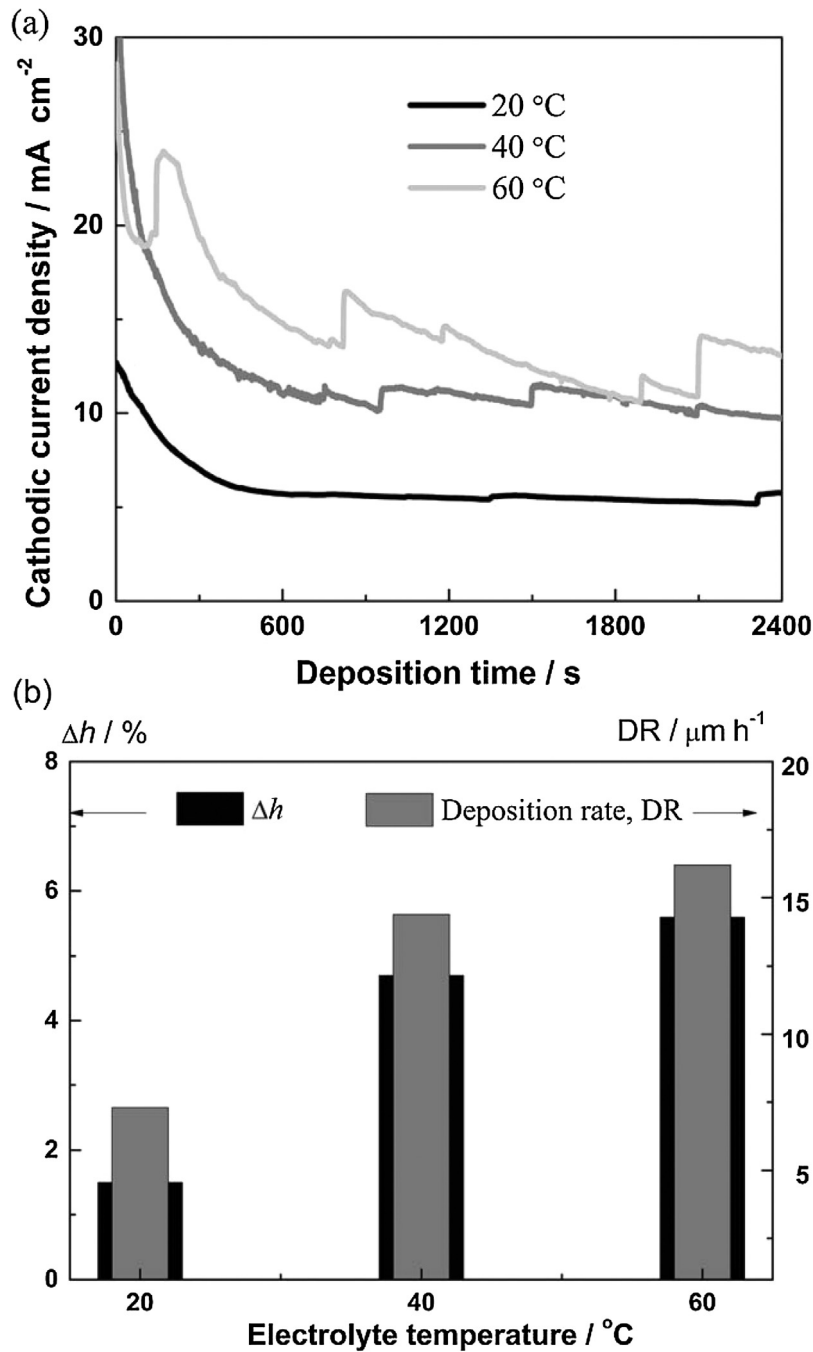


Fig. 2. (a) Chronoamperograms of Co-W mesowires deposition into AAO at pH=5, $E = -0.87$ V, and different temperatures. (b) Thickness deviation (Δh) and deposition rate (DR) as a function of temperature.

2.2. Characterization of CoW mesowires' length, composition and structure

Cross-section images were obtained using scanning electron microscopy (SEM) (Philips XL30) at 30 kV, to obtain an enhanced contrast and have a clearer view of the length of the deposited alloy wires within the template. The cross-section SEM images might give the false impression that some of the pores remain unfilled and/or the wires are broken (i.e., they are not continuous). This stems from the fact that the AAO/CoW composite was manually broken so that the cut did not leave a flat surface underneath. Some

wires or pieces of them were likely torn apart during breaking. The W content in the wires was determined by energy-dispersive X-ray (EDX) spectroscopy.

The uniformity of mesowires length in the arrays was estimated based on SEM cross-section images. The length deviation (Δh) from average (l_{avg}), maximum (l_{max}) and minimum (l_{min}) values of Co-W wires length was determined as:

$$\Delta h = \frac{((l_{max} - l_{avg}) + (l_{avg} - l_{min}))}{2 \cdot l_{avg}} \cdot 100\% \quad (1)$$

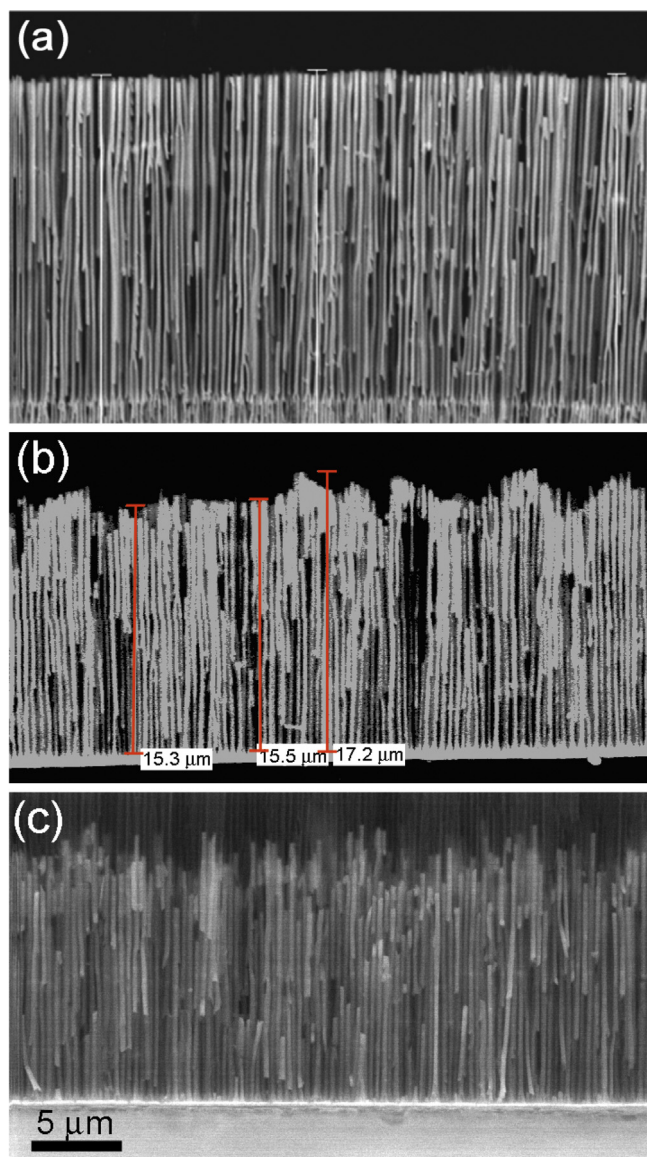


Fig. 3. SEM cross-section images of Co-W mesowires obtained by potentiostatic deposition at -0.87 V, pH=5 and temperature: (a) 20 °C, (b) 40 °C, and (c) 60 °C.

The current efficiency (CE) was calculated using the following expression:

$$CE = \frac{H_m}{H_t} 100\% \quad (2)$$

where H_m is the length of the mesowires measured from SEM images, H_t is the theoretical length of the mesowires calculated using the Faraday's law under assumption that the overall density of the alloy additively comprises densities of pure components. Current density was calculated assuming a porosity percentage of 50%.

Co-W mesowires were released from the AAO template in 10 wt % NaOH at 80 °C during 5 min and rinsed afterwards in ethanol for transmission electron microscope (TEM) observations. Prior to imaging in TEM (Jeol-JEM 2011, 200 kV), the mesowires were dispersed onto a holey carbon-coated Cu support grid. Selected area electron diffraction (SAED) patterns were taken on different mesowires in order to determine the crystallographic structure.

2.3. Magnetic characterization

Hysteresis loops were acquired at room temperature using a vibrating sample magnetometer from Oxford Instruments, applying a maximum magnetic field of 10 kOe. The loops were measured on the mesowires still embedded in the AAO templates, applying the field both along and perpendicular to the wire long axis direction. Calculations of the average interwire dipolar fields were performed taking into account the mean mesowire dimensions and the interwire distance.

3. Results and discussion

3.1. Study of electrochemical growth of Co-W mesowires

3.1.1. Potentiostatic/galvanostatic deposition under direct-current (DC) mode

During galvanostatic electrodeposition, the current densities applied earlier [33,34] for the growth of Co-W on flat surfaces or into wafers having recesses of micrometric lateral sizes cannot be transferred “automatically” to the case of electrodeposition inside meso/nanopores. One cannot expect to obtain the same results because of at least two different reasons: (1) peculiarities of diffusion into the recesses at the mesoscale, and (2) the width of pores in industrial AAO membranes is uneven—smaller width at the bottom and larger toward the top—hence resulting in a dynamic change of working area during the electrodeposition. The latter can be overcome to some extent by using potentiostatic rather than galvanostatic electrodeposition. Indeed, this mode has been used in the present study to determine the current densities that render uniform Co-W mesowires.

Similarly to what was observed in micro-scaled wafers [34], electrodeposition inside the mesopores under potentiostatic conditions at 60 °C, using relatively negative potentials and high pH (6.7 or 8.0), results in a strong influence of hydrogen evolution and concomitant alkalization at the electrode neighborhood. In these conditions, a non-uniform growth of Co-W arrays of poor quality is obtained. Better uniformity in the mesowires length was achieved at pH=5, when hydrogen evolution and alkalization of the near electrode space were minimized at the expense of decreasing the W content in the alloy. However, even at pH=5, deposition carried out at high negative potential reveals abundant hydrogen evolution and low uniformity of the mesowire arrays (Fig. 1).

The chronoamperograms for Co-W wire arrays deposited at pH=5 and fixed low cathodic polarization of -0.87 V are shown in Fig. 2(a) for different electrolyte temperatures. A decrease in temperature leads to less current fluctuations arising from hydrogen evolution. This favors higher uniformity of the electrodeposited Co-W arrays. Indeed, surveillance of length deviation (Fig. 2(b)) reveals that a lower electrolyte temperature assures not only lower hydrogen evolution, but also lower alloy deposition rates and, as a consequence, more uniform arrays of mesowires (Fig. 3). In all cases, the composition of the alloys was close to Co_{95}W_5 at.%, as determined by EDX.

Electrodeposition under galvanostatic control leads to the same tendency as for potentiostatic conditions, namely at higher current densities the growth is disturbed by hydrogen evolution. The best uniformity at 20 °C is achieved at a cathodic current density of -6 mA cm^{-2} , which roughly corresponds to potentiostatic electrodeposition at -0.87 V (Fig. 4). Galvanostatic deposition at low current densities allows better control of Co-W electrodeposition. Note that the calculated apparent partial current density for metallic phase deposition obtained at -12 mA cm^{-2} is probably overestimated, because some pores were blocked by hydrogen and became inaccessible for electrodeposition.

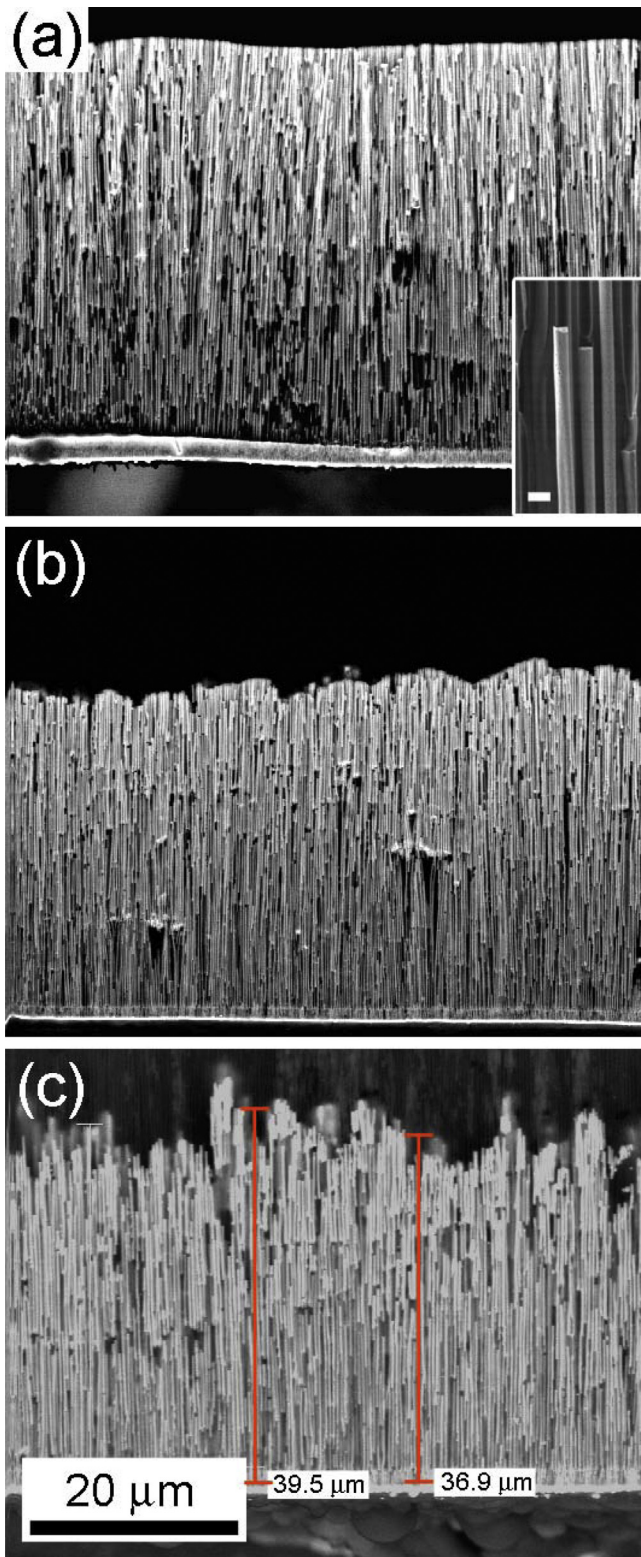


Fig. 4. SEM cross-section images of Co-W mesowires obtained by DC at pH = 5 and 20 °C under the following cathodic current densities and deposition times: (a) -6 mA cm^{-2} , 21600 s; (b) -7.5 mA cm^{-2} , 21600 s; (c) -12 mA cm^{-2} , 7200 s. The inset in (a) is a zoomed detail of a few mesowires (scale bar 400 nm).

As aforementioned, deposition proceeds in a more controlled manner only at relatively low cathodic potentials or current densities. This might be explained by peculiarities of diffusion inside the pores of the AAO template. Indeed, the presence of an

array of cylindrical pores on the electrode has a significant effect on the diffusion [35]. When a metal is deposited inside nano- or mesopores, natural convection does not take place inside the pores due to the limited cross-section. Instead, metal ions are supplied by linear diffusion. Note that, regardless the mechanism for Co(II) discharge, all the forms of Co(II) complexes participate in the mass transfer. The most probable diffusion limitations encountered during Co-W deposition in the pores were estimated using a simplified model of mass transfer in the pores.

The highest diffusion rate is to be observed when the concentration at the bottom surface of the pores with length l is equal to zero: $C(t)_{x=0} = 0$. In this case, diffusion undergoes in accordance with the second Fick's law. Under potentiostatic conditions, the concentration dependence on distance (x) and time (t) follows the Cottrell equation:

$$C_0(x, t) = C_0^* \operatorname{erf} \left[\frac{x}{2\sqrt{D_0 t}} \right] \quad (3)$$

where “erf” is an error function; C_0^* is the bulk concentration of metal ions; D_0 is the diffusion coefficient of metal complexes; and t denotes the time.

Actually, D_0 values for specific metal complexes are not easily available and should be often estimated. Very small ligands (e.g., inorganic anions) replace water molecules in the inner hydration shell of the metal ion. The net difference between the D_0 values of the hydrated metal and the complex may be then rather small. Actually, they can be assumed to be equal, which is an acceptable approximation. Note that when the hydration shell is completely replaced by small hydrophobic anions like Cl^- , the diffusion coefficient of the complex may become significantly greater than that of the hydrated ion. As the ligand size increases, the D value of the complex tends toward that of the ligand [36]. For our simulations we used a value of apparent diffusion coefficient for Co citrate complexes of $7.9 \cdot 10^{-7} \text{ cm}^2 \text{ s}^{-1}$ [37,38], i.e. the diffusion coefficient of cobalt due to complexation is 3 times lower than that reported in the literature for Co(II) in sulfate-ammonia solutions [39]. Also, the partial blocking of electrode surface by intermediates may have an influence on the apparent value of the diffusion coefficient [38].

In Fig. 5 the concentration $C(x, t)$ at $x = 0.25l$, $x = 0.5l$, $x = 0.75l$, and $x = l$ for $C_0^* = 0.20 \text{ M}$ as a function of time is shown. Although both W(VI) and Co(II) are present in the electrolyte, only Co(II) was considered because of the low tungsten content in the alloy. Indeed, considering the relatively low current densities used, partial hydrogen evolution current density is in all cases smaller than -20 mA cm^{-2} . In these conditions, the thickness of the diffusion layer at H_2 -evolving horizontal electrode is 40–80 μm [40], which is comparable to the length of the pores. Therefore, the Nernst's diffusion layer concept and the Cottrell equation can be safely applied. The model reveals that the concentration gradient at the top of the pores is significant, i.e. $C(x = l, t_x) < C_0^*$ already after 4 seconds from the beginning of the electrodeposition. Simultaneously, the maximum current density which can be supported by diffusion can be calculated by Cottrell's equation for current response:

$$i_d(t) = nFC_0^* \sqrt{\frac{D_0}{\pi t}} \quad (4)$$

After 4 seconds diffusion from the bulk of solution toward the pores takes place and finally a stationary flux of metal ions can be settled:

$$\left[\frac{\partial C_0(x, t)}{\partial x} \right]_{x=0} = \left[\frac{\partial C_0(x, t)}{\partial x} \right]_{x=l} \quad (5)$$

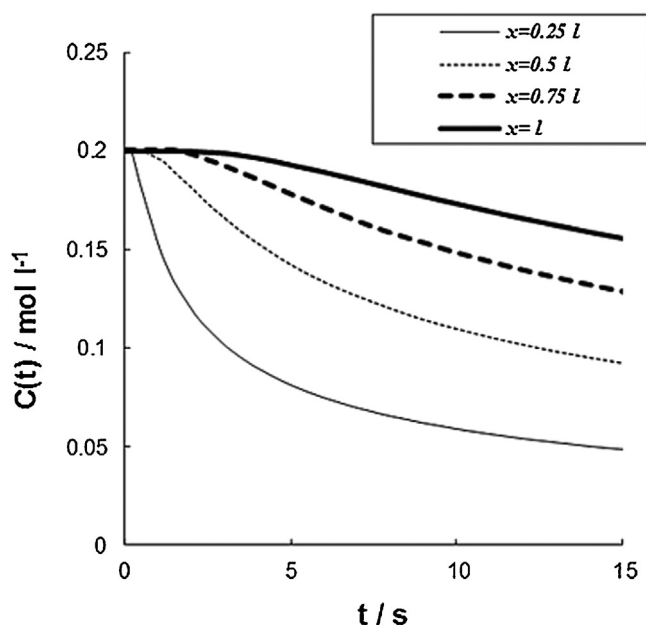


Fig. 5. Concentration of metal ions, i.e. Co(II), as a function of time at various distances (x) from the bottom of the pores, as calculated using eq. (3); $l = 60 \mu\text{m}$, $D_0 = 7.9 \times 10^{-7} \text{cm}^2 \text{s}^{-1}$, $C_0^* = 0.20 \text{M}$.

and:

$$i_d = \frac{nFC_0^*D_0}{l} \quad (6)$$

The equation describing the time needed to switch from non-stationary to stationary diffusion (t_{tr}) regimes can be derived from the equality between eq. (4) and (6):

$$t_{tr} = \frac{l^2}{D_0\pi} \quad (7)$$

In the studied case with pore length $l = 60 \mu\text{m}$, the value of t_{tr} calculated from eq. (7) is 14.3 s, and the diffusion current calculated using eq. (4) or (6) is equal to 5.1mA cm^{-2} . At this point it should be clarified that diffusion is spherical at the top of the pores ('outer layer') but remains planar inside the AAO pores. If only spherical diffusion is to be assumed, the resulting current density is more than 150 times the actual value. Therefore, the 'outer' diffusion layer is likely to be very thin. The calculated value (5.1mA cm^{-2}) is close to the one obtained at 20°C on the experimental chronoamperograms shown in Fig. 2(a). This agreement indicates that the electrodeposition of Co-W mesowires in our conditions is limited by mass transfer even at relatively low current densities. In other words, electrodeposition of the mesowires is governed by the diffusion of discharging metal-containing species from the bulk solution toward the pores, whereas Co and Co-W electrodeposition on flat electrodes proceeds under kinetic limitations [38]). This can be additionally proven by the current increase with temperature (see Fig. 2(a)), as higher activation energy holds under kinetic limitations in comparison with diffusion processes.

3.1.2. Pulse current (PC) deposition

Pulse deposition is often used to improve the control over the electrochemical process and, in turn, on the properties of electrodeposits such as morphology, crystallite size, chemical composition, crystalline structure and/or hydrogen inclusion [41–43]. By changing the frequency (or duty cycle) it is possible

to provide either kinetic or diffusion (or mixed) control of electrode reaction. The kinetics of codeposition of W with Co (and other group metals) is rather complicated [38,44] because of the adsorption of intermediates and solution components (e.g. ligands) on the electrode, coupled with charge transfer and diffusion processes. Therefore, it is impossible to distinguish in experimental electrochemical impedance (EIS) spectra, frequency ranges for which only the kinetics or the mass transfer control electrode processes apply [38,45]. Simulation of EIS is a convenient way to estimate frequencies for which diffusion or kinetic limitations take place. In particular, diffusion gives rise to the occurrence of Warburg impedance. The simulation performed in this study was restricted to a Randles-Ershler equivalent circuit containing the following elements: solution resistance, double layer capacitance (Q_{dl}), faradaic charge transfer resistance (R_{ct}), and Warburg impedance. This impedance depends on the frequency of the potential perturbation and mass transfer conditions (concentrations, diffusion coefficients, and type of diffusion—semi-infinite or bounded diffusion). At high frequencies the Warburg impedance is small since diffusing reactants do not have to move very far; at low frequencies the reactants have to diffuse farther, thereby increasing the Warburg impedance. The typical shape of the Nyquist diagram for Randles-Ershler impedance is shown in Fig. 6 (a). At a critical frequency (ω_{crit}) the control over the electrochemical reaction switches from kinetic to diffusion and vice versa.

For numerical simulations the values of circuit elements determined in [38] were used. A double layer capacitance of $1 \mu\text{F cm}^{-2}$ ($n=0.85$) was employed. To calculate the Warburg constant, the diffusion of main components in citrate solution at $\text{pH}=5$ were considered: CoHCitr^- (as oxidant) and all forms of citrates HCitr^- (as reductant). Taking into account that $[\text{Co}^{2+}] = 0.20 \text{M}$, the concentration of all the forms of citrate in the diffusion layer is 0.20M [44]. Their diffusion coefficient was taken as $D_{citr} = 5.9 \cdot 10^{-6} \text{cm}^2 \text{s}^{-1}$ [46], thus the Warburg coefficient is equal to $\sigma = 0.3614 \Omega \text{cm}^2 \text{s}^{-1}$. Finally, the values of R_{ct} depend on the deposition potential and vary from $6544 \Omega \text{cm}^2$ (at low polarization, i.e., in the range from -0.70 to -0.55V) to $226 \Omega \text{cm}^2$ (at high polarization, e.g., -0.86V). The calculated dependence of charge transfer resistance (R_{ct}) on the values of ω_{crit} is presented in the insert of Fig. 6(a). Numerical simulation revealed that the values of ω_{crit} depend mainly on the values of R_{ct} and σ . Namely, the higher the charge transfer resistance, the lower the value of ω_{crit} , i.e. the transition from kinetics control to diffusion control occurs at lower frequencies. In our Co-W electrolyte, $\omega_{crit} \leq 0.3 \text{Hz}$ in all cases. This means that at higher frequencies the electrode processes are controlled by charge transfer rate, whereas at lower frequencies diffusion is governing the process. Fig. 6(b) and (c) display the EIS spectra in Nyquist and Bode coordinates, respectively, recorded during electrodeposition of Co-W at $\text{pH} 6.7$ and $E = -0.8 \text{V}$ inside mesopores of 200nm in diameter. The experimental spectra are described by an equivalent circuit (inset of Fig. 6(c)) containing an adsorption stage. Elements take the following values: $R_1 = 9.83 \Omega \text{cm}^2$; $R_2 = 535 \Omega \text{cm}^2$; $\text{CPE1} = 0.0021 \text{F cm}^{-2}$ ($n = 0.63$); $\text{CPE2} = 0.00715 \text{F cm}^{-2}$ ($n = 0.60$); $R_3 = 104 \Omega \text{cm}^2$. The large capacitance values are probably caused by the formation of unevenly distributed oxide-containing intermediates on the surface.

For electrodeposition in PC mode, pulse durations of 4 ms, 20 ms, 200 ms, and 2000 ms were applied. These correspond to sinusoidal frequencies of 125 Hz, 25 Hz, 2.5 Hz, and 0.25 Hz, respectively, for a duty cycle of 50%. Taking into account that the concentration gradient decreases during the rest time, it is possible to state that the electrode process is controlled by the kinetics of charge transfer reaction even at the longest pulse duration applied (2000 ms).

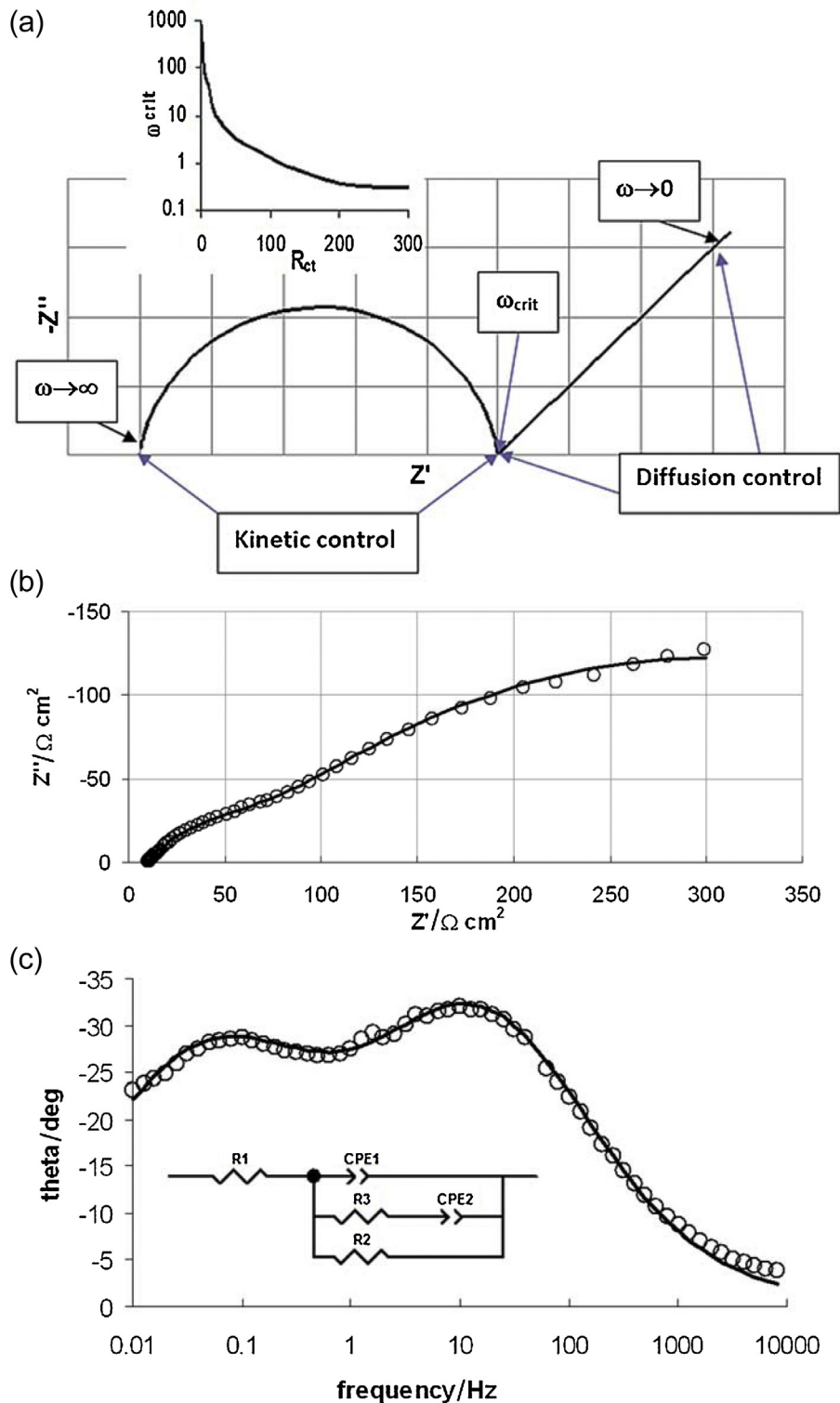


Fig. 6. (a) Nyquist diagram for Randles circuit including semi-infinite linear diffusion. Insert presents the calculated dependence of ω_{crit} on charge transfer resistance (R_{ct}). Values of circuit elements are indicated in the text. Experimental (open circles) and fitted (solid line) EIS spectra in (b) Nyquist and (c) Bode coordinates recorded during Co-W electrodeposition at pH 6.7 and $E = -0.8 \text{ V}$ inside mesopores of 200 nm in diameter. Inset in (c) is the equivalent circuit. R1 is uncompensated resistance; R2 is charge transfer resistance; CPE1 is constant phase element of double electric layer; R3 and CPE2 are adsorption resistance and constant phase element (capacity), respectively.

Electrodeposition at pulse cathodic current densities (i_{on}) within the range of $-i = 7.5 - 60 \text{ mA cm}^{-2}$ and at a duty cycle of 20–50% was investigated. The characteristic influence of pulse duration on the uniformity of mesowires growth is shown in Fig. 7. The most uniform growth was obtained for the shortest pulse duration (4 ms). Likewise, the effect of duty cycle is shown in Fig. 8.

Uniformity worsens at high duty cycles (i.e. 50% and 33%) probably because the pause duration is exceedingly short to allow the hydrogen bubbles to be released from the template while a new portion of electrolyte penetrates inside the pores from the bulk of the solution. In addition, mass transport limitation is neglected at shorter pulses and smaller duty cycles (equivalent to high

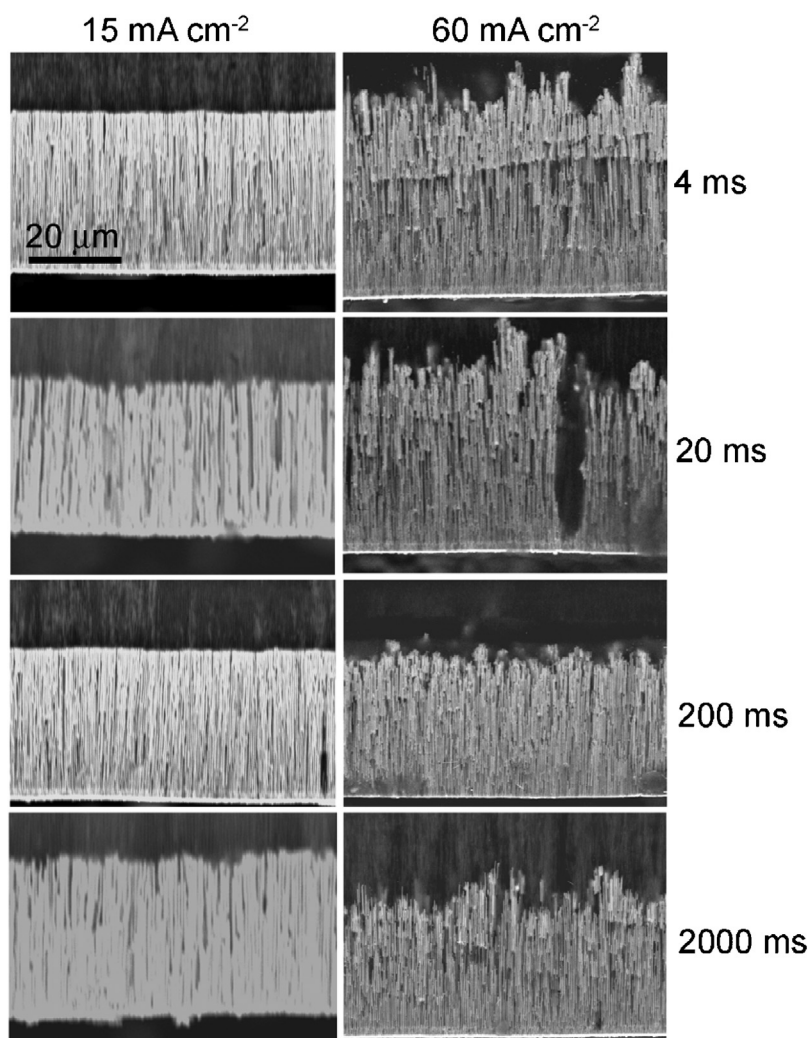


Fig. 7. Pulse duration effect. SEM cross-section images of Co-W mesowires obtained under PC deposition at pH = 5, 20 °C, duty cycle of 20%, and different t_{on} times. Deposition time was 28800s at $i_{on} = -15 \text{ mA cm}^{-2}$ and 7200s at $i_{on} = -60 \text{ mA cm}^{-2}$.

frequencies). It should be mentioned that with increasing the pause duration mesowires grow in a more uniform manner, but the total duration of electrodeposition to obtain the same length of mesowires also increases. In addition, for a large pulse current density and pulse duration, the average current density exceeds the limiting diffusion current, which is equal to $\sim 5 \text{ mA cm}^{-2}$ under our deposition conditions, composition of solution, and geometry of pores (see section 3.1.1). Therefore, in this case hydrogen evolution dominates.

Furthermore the duty cycle has an impact on the tungsten content along the wires (i.e., compositional homogeneity) (Fig. 9). For a given current density, at lower duty cycle (which means longer pause duration) the tungsten content along the mesowires is much more homogeneous.

3.2. Structural characterization of Co-W mesowires

Fig. 10 shows representative TEM images of Co-W wires deposited by DC and PC conditions. The mesowires were of nanocrystalline nature and exhibited the hexagonal close-packed (hcp) structure, independently of the electrodeposition conditions and final wire length (see SAED patterns in Fig. 10b and d). This was to some extent expected given the low W content (below 6 at.%) in

all the wires (Fig. 9). It is known that amorphization in electrodeposited Co-W films typically takes place for higher W contents (> 30 at.%) [33]. Also it is known that the face-centered cubic (fcc) phase of Co is promoted during electrodeposition of nanowires only for rather acid pH values, close to pH 2 [12,47], which is not the case of our study. Finally, according to the Co-W binary phase diagram, W is also stabilizer of the hcp phase when dissolved in small amounts into Co [48].

Remarkably, although the conditions corresponding to the mesowire in Fig. 10(a) were the best ones within the DC regime, residual porosity was noticed both by TEM and SEM. This porosity stems for the hydrogen co-evolution that accompanies metal ions discharge. Meanwhile, wires obtained by PC deposition looked more compact. The measured lengths were in agreement with the values previously determined by SEM.

3.3. Magnetic properties

Hysteresis loops were recorded on selected arrays of mesowires, still embedded in the AAO templates, prepared under both direct current and pulse plating conditions. The selected samples correspond to deposition at pH=5 and 20 °C, with optimum conditions to attain homogeneous filling of the pores. Two

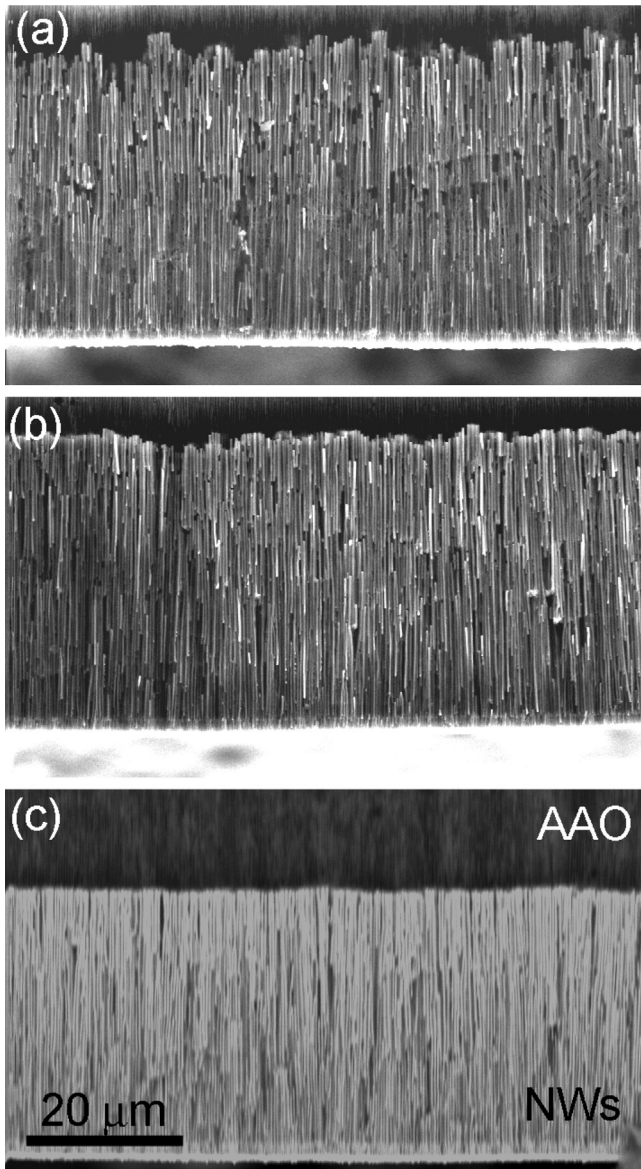


Fig. 8. Duty cycle effect. SEM images of Co-W mesowires obtained by PC deposition at pH = 5, 20 °C, $i_{on} = -15 \text{ mA cm}^{-2}$, $t_{on} = 4 \text{ ms}$, and different duty cycle and deposition time: (a) 50%, 11632 s; (b) 33%, 17448 s; and (c) 20%, 28800 s.

different sets of mesowires were grown by DC and PC, with different lengths, to compare the properties of short (about $1 \mu\text{m}$ long) versus long (about $25 \mu\text{m}$ long) mesowires.

Representative hysteresis loops, measured along and perpendicular to the mesowire axes, are shown in Fig. 11. The values of coercivity, H_C , for the different investigated samples are listed in Table 1. Since all samples are polycrystalline (hcp structure) and contain a similar W content (3–5 at.%), it is unlikely that the slight variations in microstructure/composition can explain the observed changes in H_C . Table 1 reveals that, in fact, H_C decreases when the length of the mesowires is increased. Such inverse relationship between H_C and sample/particle size is typical of ferromagnetic materials and has been observed also in other metallic nanowires systems [49]. In ferromagnetic alloys, H_C usually increases when the particle size is reduced due to a transition from a multi-domain to a mono-domain magnetic configuration, where only coherent rotation of the magnetic moments (but not propagation of domain

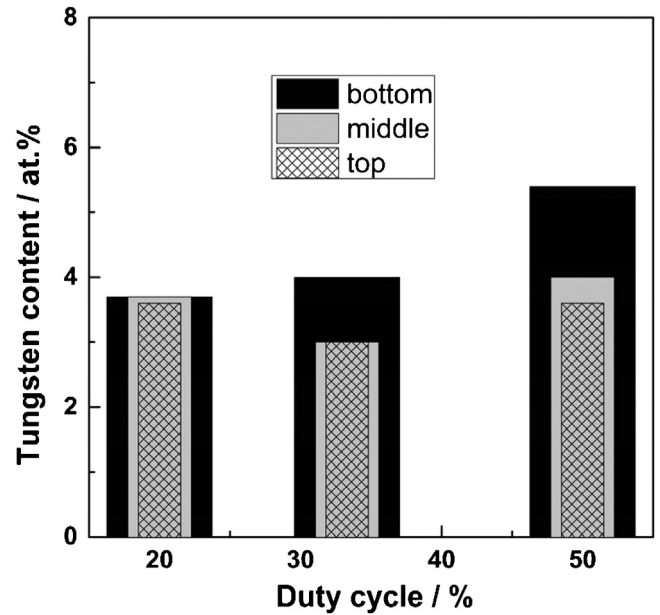


Fig. 9. Dependence of tungsten content in Co-W wires as a function of the duty cycle at pH = 5, 20 °C, $i_{on} = -15 \text{ mA cm}^{-2}$, and $t_{on} = 4 \text{ ms}$.

walls) takes place during magnetization reversal. However, no pronounced changes in the domain structure are anticipated between the two sets of short or long mesowires. Actually, in a first approximation, the mesowires can be considered to behave as magnetic dipoles. In arrays of nanowires, the existence of magnetic dipolar interactions between the wires has been reported to have a net effect on H_C [50]. Typically, H_C decreases with an increase of magnetic dipolar interactions. These interactions mainly depend on the mesowires aspect ratio and the average interwire distance. Moreover, H_C is larger when measured along the wires axis (\parallel), as compared to hysteresis loops recorded along the perpendicular-to-the-wires axis (\perp). This can be ascribed to the trade-off between the effective shape anisotropy of the mesowires and the net role of interwire dipolar interactions. It is remarkable that the measured values of H_C in the Co-W mesowires are larger than those of pure fcc-Co or hcp-Co for wires with similar diameter and aspect ratio and interwire distance, where H_C typically ranges between 100 and 250 Oe [27,47,49,50].

Isolated polycrystalline mesowires with a large aspect ratio should exhibit a square hysteresis loop when the magnetic field is applied parallel to the wires axis and a tilted hard-axis loop along the perpendicular direction, due to the shape anisotropy [50–53]. Conversely, the investigated arrays of Co-W wires exhibit sheared hysteresis loops along both directions of measurement. Such behavior can be ascribed to the existence of interwire magnetic dipolar interactions; more specifically, to the competition between shape anisotropy, magnetocrystalline anisotropy and the dipolar fields created between neighboring wires. Fig. 11 reveals that for the shortest mesowires, the magnetic easy axis in the array remains the one along the mesowire axis, where slightly larger M_R/M_S and H_C values are obtained with respect to the measurements acquired applying the field along the perpendicular-to-the-wire direction. Conversely, such a trend is lost for the long mesowires, where the loops along both directions of measurement virtually overlap.

For a two-dimensional infinite array of cylindrical particles with radius r , length L , aspect ratio $A_r = L/2r$ and interwire distance D , the total dipolar field created when all wires are oriented along the

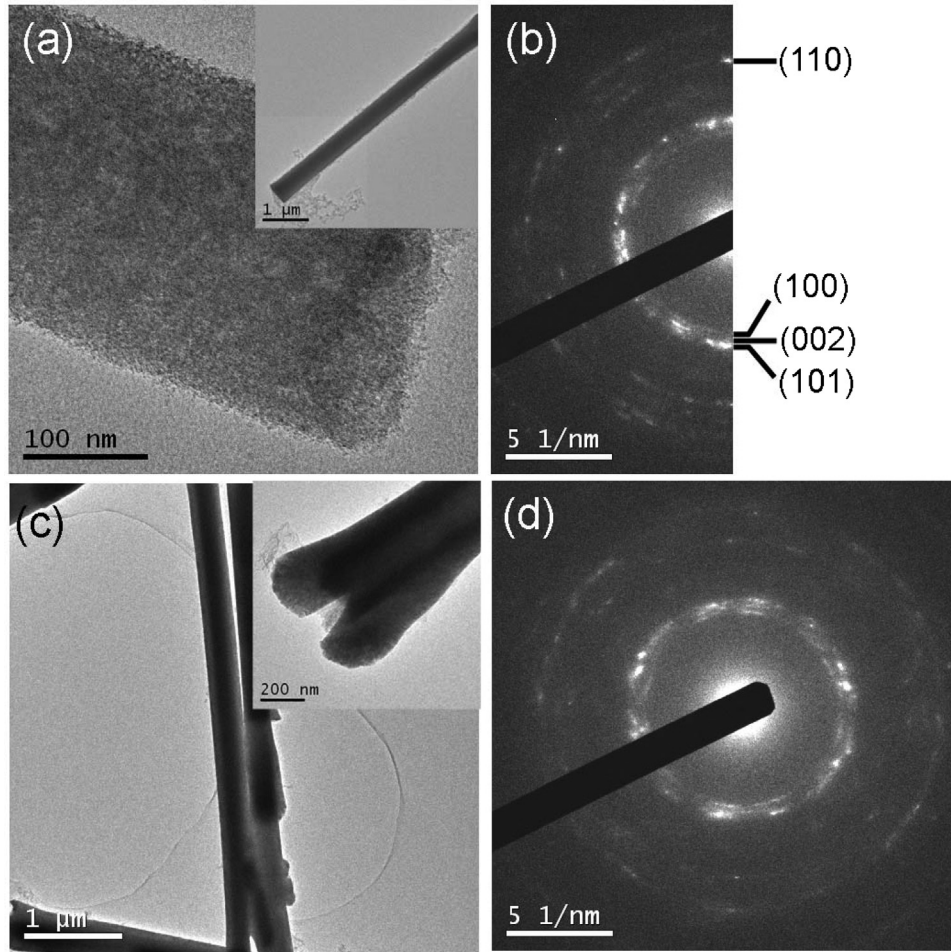


Fig. 10. (a) TEM image of the end of a mesowire and (b) corresponding SAED pattern for Co-W wires obtained by DC mode at -6 mA cm^{-2} for 14400 s (pH = 5, 20°C). (c) TEM image of a bundle of Co-W wires obtained by PC deposition at $i_{on} = -15 \text{ mA cm}^{-2}$, $t_{on} = 4 \text{ ms}$. The insets in (a) and (c) show a less magnified view of the wire and the bottom part of a wire showing the typical branched structure, respectively. The overall length of the mesowires is $40 \mu\text{m}$ in both cases.

wire axis direction can be written as [27,49,51]:

$$H_{\text{dip},0^\circ} = \frac{4.2M_s\pi r^2L}{D^3} \quad (8)$$

If all moments are aligned perpendicular to the wires direction, then the dipolar field would be:

$$H_{\text{dip},90^\circ} = \frac{2.1M_s\pi r^2L}{D^3} \quad (9)$$

In turn, the self-demagnetizing field of one wire can be expressed as:

$$H_{\text{demag}} = (N_\perp - N_\parallel)M_s \quad (10)$$

where N_\parallel and N_\perp are the demagnetizing factors along the wire axis and its perpendicular direction and can be calculated using a prolate spheroid approximation, as follows [54]:

$$N_\parallel = \frac{4\pi}{A_r^2 - 1} \left[\frac{A_r}{2\sqrt{(A_r^2 - 1)}} \ln \left(A_r + \sqrt{A_r^2 - 1} \right) - 1 \right] \quad (11)$$

$$N_\perp = \frac{4\pi - N_\parallel}{2} \quad (12)$$

Hence, the total effective anisotropy field can be then expressed as:

$$H_{K,\text{eff}} = (N_\perp - N_\parallel)M_s - \frac{6.3M_s\pi r^2L}{D^3} + H_{mc} \quad (13)$$

Here H_{mc} is the magnetocrystalline anisotropy contribution, which for single-crystalline hcp-Co is negative and is approximately equal to $5 M_s$ [27]; for polycrystalline mesowires, H_{mc} averages out and is close to 0. Equation 13 predicts that if $H_{K,\text{eff}}$ is positive the magnetic easy axis will be to the wires axis; otherwise, for negative $H_{K,\text{eff}}$ the magnetic easy axis will tend to be oriented along the \perp direction [49]. If one uses approximate values of: wire length, wire diameter and distance between wires (pitch size), one can try to estimate the effective anisotropy field of a given array of mesowires. Alternatively, one can determine a critical mesowire length, L_c that would render $H_{K,\text{eff}} = 0$, i.e., the critical length beyond which the effective anisotropy direction would switch from the \parallel to the \perp directions. Considering that $(N_\perp - N_\parallel) \approx 2\pi$, $r = 120 \text{ nm}$, $D = 450 \text{ nm}$ (as estimated from SEM images of the AAO template) and that our material is mainly hcp-Co (i.e., $0 < H_{mc} < 5 M_s$, depending on the degree of polycrystallinity), Equation 13 then predicts that L_c will range from approximately $0.5 \mu\text{m}$ to $2 \mu\text{m}$. Hence, this simplified reasoning provides a semi-quantitative explanation of why the effective easy axis along the \parallel direction in the arrays of short mesowires is lost for the case of the longer mesowires.

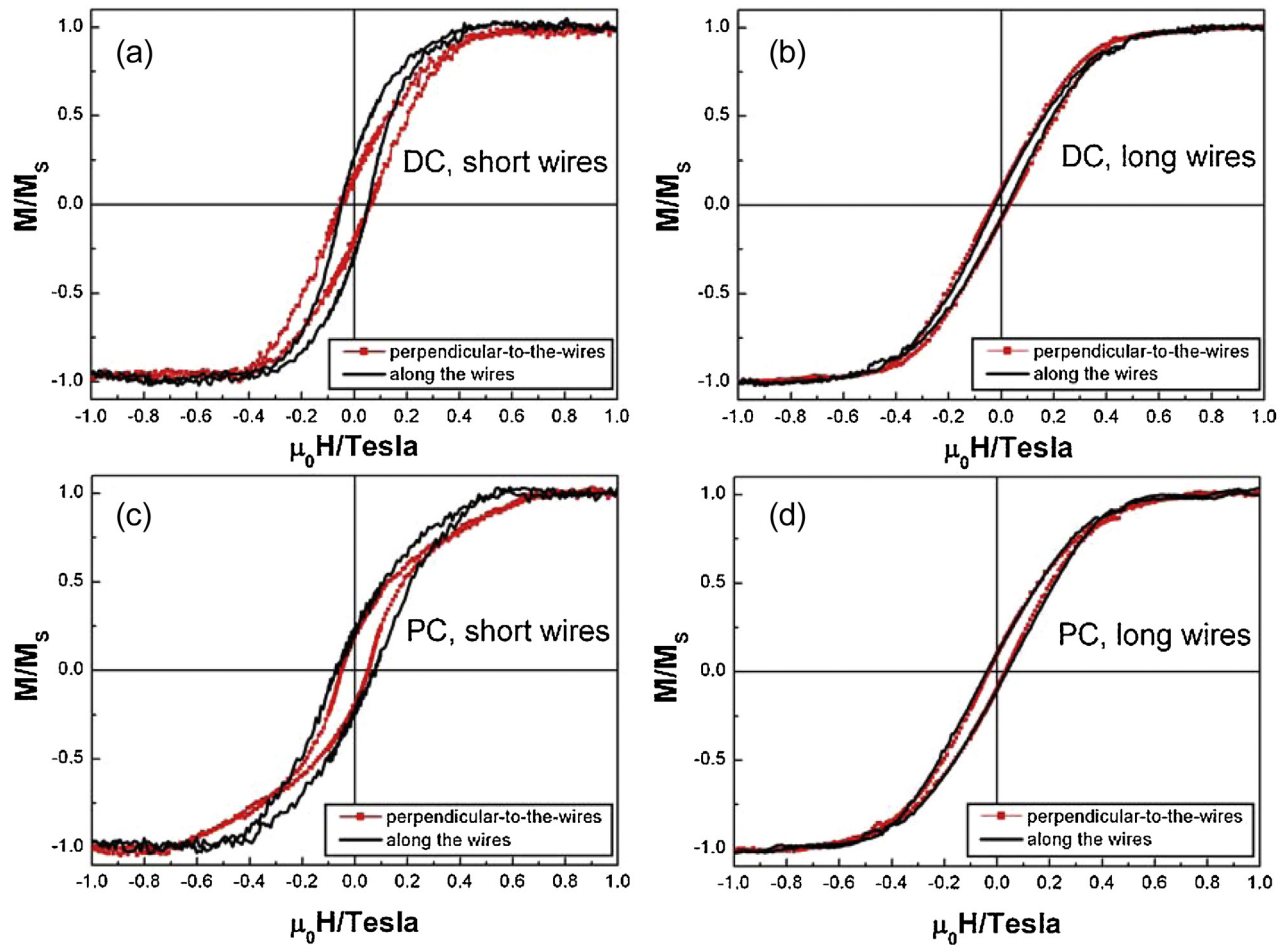


Fig. 11. Hysteresis loops of selected arrays of mesowires (embedded in the AAO templates), grown by DC (a,b) and PC (c,d) conditions, applying the external magnetic field along and perpendicular to the wires direction. Panels (a) and (c) correspond to short mesowires ($\sim 1 \mu\text{m}$ long) whereas panels (b) and (d) show the loops of longer mesowires ($\sim 25 \mu\text{m}$ long).

Table 1

Summary of the magnetic properties of Co-W wire arrays.

Current mode	Wires length, μm	$H_c \perp$ (Oe)	H_c (Oe)	M_R/M_S \perp	M_R/M_S
DC, -6 mA cm^{-2} , short	1.2	499	499	0.21	0.28
PC, $i_{on} = -15 \text{ mA cm}^{-2}$, $t_{on} = 4 \text{ ms}$, short	0.8	510	730	0.20	0.23
DC, -6 mA cm^{-2} , long	26.0	264	234	0.08	0.07
PC, $i_{on} = -15 \text{ mA cm}^{-2}$, $t_{on} = 4 \text{ ms}$, long	22.0	350	365	0.09	0.09

4. Conclusions

The main conclusions of the present study can be summarized as follows:

1. The best filling of AAO mesopores by Co-W alloy was obtained at room temperature using $\text{pH}=5$: in DC mode at low current densities or polarizations; in PC mode at shorter pulse durations and smaller duty cycles, i.e. under conditions at which the influence of diffusion is minimized.
2. Under direct current or potential mode the electrode process undergoes under kinetic control on flat surfaces whereas the process is limited by mass transfer during electrodeposition in the mesopores. For the membranes used in this work (pore

length about $60 \mu\text{m}$, pore diameter 240 nm) the following diffusion processes were revealed: after 4 s from the beginning of electrodeposition the diffusion from the bulk of the solution toward the pores starts and after $\sim 14 \text{ s}$ diffusion evolves from non-stationary to stationary. Under PC mode the Co-W electrodeposition process is controlled by kinetics at frequencies $>0.3 \text{ Hz}$; and by diffusion at lower frequencies.

3. The magnetic properties of selected arrays of mesowires (the ones grown under optimum conditions for homogeneous filling of the pores) reveal a semi-hard ferromagnetic behavior and a strong influence of interwire magnetic dipolar interactions on the resulting shape of the hysteresis loops. While a clear magnetic easy direction along the mesowires long axis is observed for short mesowires, such a trend is lost for longer mesowires. The interplay between shape anisotropy,

magnetocrystalline anisotropy and the dipolar fields created between neighboring wires can explain this observation.

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